## Creep and Mechanical Properties of  $Cu<sub>6</sub>Sn<sub>5</sub>$  and  $(Cu,Ni)<sub>6</sub>Sn<sub>5</sub>$ at Elevated Temperatures

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 $Cu<sub>6</sub>Sn<sub>5</sub>$  is the most common and important intermetallic compound (IMC) formed between Sn-based solders and Cu substrates during soldering. The  $Cu<sub>6</sub>Sn<sub>5</sub>$  IMC exhibits significantly different thermomechanical properties from the solder alloys and the substrate. The progress of high-density threedimensional (3D) electrical packaging technologies has led to increased operating temperatures, and interfacial  $Cu<sub>6</sub>Sn<sub>5</sub>$  accounts for a larger volume fraction of the fine-pitch solder joints in these packages. Knowledge of creep and the mechanical behavior of  $Cu<sub>6</sub>Sn<sub>5</sub>$  at elevated temperatures is therefore essential to understanding the deformation of a lead-free solder joint in service. In this work, the effects of temperature and Ni solubility on creep and mechanical properties of  $Cu<sub>6</sub>Sn<sub>5</sub>$  were investigated using energy-dispersive x-ray spectroscopy and nanoindentation. The reduced modulus and hardness of  $\rm Cu_6Sn_5$  were found to decrease as temperature increased from  $25^{\circ}\rm C$  to 150°C. The addition of Ni increased the reduced modulus and hardness of  $Cu<sub>6</sub>Sn<sub>5</sub>$  and had different effects on the creep of  $Cu<sub>6</sub>Sn<sub>5</sub>$  at room and elevated temperatures.

Key words: Intermetallic compounds, nanoindentation, mechanical properties, lead-free solder

## INTRODUCTION

The continuous performance demands and progress of three-dimensional (3D) electrical packaging technologies has led to increased Joule heating and accompanying operating temperature<sup>1</sup> of lead-free solder joints. Moreover, the volume fraction of IMCs in a typical lead-free solder joint has increased, and interfacial IMCs account for a larger fraction of the joint microstructure because of the minimization of solder joints in 3D integrated circuits  $(ICs)<sup>2</sup>$ . The diameter of a solder joint in a traditional ball grid array (BGA) is typically around 100  $\mu$ m, although this is expected to reduce to approximately 1  $\mu$ m in 3D ICs.<sup>3</sup> In this scenario, the solder alloys can conceivably be completely consumed and a solder joint may consist of a few grains of intermetallic compounds  $(MCs)$ .<sup>2,3</sup> As a result, the deformation

behavior of a lead-free solder joint is determined by the mechanical properties of the IMCs rather than the solder alloys.<sup>4</sup>

 $Cu<sub>6</sub>Sn<sub>5</sub>$  is an important intermetallic compound (IMC) because it is commonly formed during interface reactions between most Sn-based solders and Cu substrates.<sup>5</sup> For solder joints in 3D ICs,  $Cu<sub>6</sub>Sn<sub>5</sub>$ is expected to be the dominant phase in the joint microstructure even after the aging processes. Thus, the mechanical properties of  $Cu<sub>6</sub>Sn<sub>5</sub>$  play a determinant role in the overall deformation of a solder joint in 3D ICs. The mechanical properties of  $Cu<sub>6</sub>Sn<sub>5</sub>$  have been studied both experimentally and theoretically during the last decade. $6-9$  Nanoindentation has been proven as a suitable method to investigate the mechanical properties of IMCs formed in diffusion samples,  $\delta$  at the solder–substrate interface,<sup>7,9</sup> and in bulk IMCs formed by solidification and diffusion.<sup>10</sup> These previous (Received April 20, 2012; accepted August 6, 2012; Solidification and diffusion.<sup>\*\*</sup> These previous (Received April 20, 2012; accepted August 6, 2012; accepted August 6, 2012; accepted August 6, 2012; accepted August 6, 20

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